

for the drain current used, the figure provides an estimate for  $S_{ID}^{1/2}$  useful for design guidance. Possible small-geometry noise increases described in Section 3.10.2.2 are excluded in the figure.

The gate-referred thermal-noise voltage PSD,  $S_{VG}$ , shown in the MOS noise model of Figure 3.60, is important for many applications, including when voltage signals appear at the gate of transistor input stages.  $S_{VG}$  is found by dividing the drain-referred thermal-noise current PSD,  $S_{ID}$ , by  $g_m^2$ . This refers drain noise current PSD to a gate noise voltage PSD.

Table 3.30 summarizes expressions for  $S_{VG}$ . In the first expression,  $S_{VG}$  is expressed in terms of device  $g_m/I_D$  and  $g_m$  where the equivalent noise resistance,  $R_N$ , is inversely proportional to  $g_m$  as it was for  $S_{ID}$ .  $R_N$  corresponds to the resistance value giving thermal-noise voltage equal to that effectively

**Table 3.30** MOS gate-referred thermal-noise voltage PSD expressions and trends in terms of the inversion coefficient, channel length, and drain current. Voltage density (nV/Hz<sup>1/2</sup>) is found by taking the square root of the convenient PSD expressions

Gate-referred thermal-noise voltage PSD	$IC \uparrow$ $L, I_D$ fixed	$L \uparrow$ $IC, I_D$ fixed	$I_D \uparrow$ $IC, L$ fixed
From $g_m$ : $S_{VG} = 4kT \cdot \frac{n\Gamma}{g_m} = 4kT \left( \frac{n\Gamma}{\frac{g_m}{I_D} \cdot I_D} \right) = 4kT \cdot R_N$ $R_N = \frac{n\Gamma}{g_m}$	$\uparrow$ as $g_m/I_D$ decreases from maximum value in WI	Unchanged, but decreases if less vel. sat. reduction of $g_m/I_D$	$\downarrow \propto \frac{1}{I_D}$
Convenient expression: $S_{VG} = \frac{(4.07 \text{ nV})^2}{\text{Hz}} \left( \frac{T}{300\text{K}} \right) n\Gamma \left( \frac{1000 \mu\text{S}}{g_m} \right)$			
From $IC, L, I_D$ : $S_{VG} = 4kT \left( n\Gamma (\sqrt{IC + 0.25} + 0.5) \left( \frac{nU_T}{I_D} \right) \right)$ $= 4kT [(1/2)n^2 U_T/I_D] \text{ in WI}$ $= 4kT [(2/3)n^2 U_T \sqrt{IC/I_D}] \text{ in SI without vel. sat.}$ $= 4kT [(8/3)n^3 U_T (U_T/(LE_{CRIT}))' IC/I_D] \text{ in SI with full vel. sat.}$	Constant in WI $\uparrow \propto \sqrt{IC}$ in SI if no vel. sat. $\uparrow \propto IC$ in SI with full vel. sat.	Unchanged, but decreases if less vel. sat. reduction of $g_m/I_D$ $\downarrow \propto \frac{1}{L}$ in SI with full vel. sat.	$\downarrow \propto \frac{1}{I_D}$
Convenient expression: $S_{VG} = \frac{(2.069 \text{ nV})^2}{\text{Hz}} \left( \frac{T}{300\text{K}} \right)^2 \cdot n^2 \Gamma (\sqrt{IC + 0.25} + 0.5) \left( \frac{100 \mu\text{A}}{I_D} \right)$			
To include velocity saturation and VFMR decreases in $g_m$ , replace $IC$ with $IC(1 + IC/IC_{CRIT})$ as described in Table 3.17			

$S_{VG}$  is for saturation where  $V_{DS} > V_{DS,sat}$ .

Velocity saturation refers to both velocity saturation and VFMR effects.

$\Gamma$ , given by Equation 3.106, increases from one-half in weak inversion to two-thirds in strong inversion, excluding small-geometry increases described in Section 3.10.2.2.  $IC$  and  $L$  trends exclude small-geometry increases in  $\Gamma$ .

Convenient expressions assume  $k = 1.3806 \times 10^{-23}$  J/K.